Appendix B - Report of Preliminary Soil Borings Testing

INTRODUCTION

The following report is from the soil borings completed on the Dickinson Theodore Roosevelt Regional Airport in February of 2014. This report provides useful information on the existing pavement section subbase depth, condition, and the soils underneath the pavement section.

REPORT OF PRELIMINARY SOIL TESTING

DICKINSON THEODORE ROOSEVELT
REGIONAL AIRPORT RUNWAY EXPANSION
PROJECT #: AIP 3-38-0013-029-2013
KLJ 1513301
DICKINSON, NORTH DAKOTA

For
Attn: Mr. Charlie Baker
Dickinson Municipal Airport Authority
c/o KLJ
PO Box 1157
Bismarck, North Dakota 58502

Laboratory Number 14-019

February 27, 2014

Material Testing Services, LLC

February 27, 2014

Attn: Mr. Charlie Baker
Dickinson Municipal Airport Authority
c/o KLJ
PO Box 1157
Bismarck, North Dakota 58502

re:

PRELIMINARY SOIL TESTING
RUNWAY EXPANSION
DICKINSON THEODORE ROOSEVELT REGIONAL AIRPORT
DICKINSON, NORTH DAKOTA
LAB NO. 14-019

Dear Mr. Baker:

Enclosed is the report of the preliminary soil testing conducted at the Dickinson Municipal Airport. The work was conducted in general accordance with the solicitation for the project.

A total of 12 soil borings were drilled for the project along proposed taxiway and runway.

This report contains the logs of the borings and the evaluation of the soil conditions encountered at the site. The soil samples will be stored at the laboratory for at least 14 days from the report date at which time they will be discarded.

Please call me if you have any questions or comments concerning this report.

Sincerely,

MATERIAL TESTING SERVICES, LLC

Rusten R.L. Roteliuk, PE Geotechnical Engineer

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Report of Preliminary Soil Testing

Proposed Dickinson Municipal Airport Runway Expansion – Dickinson, North Dakota Laboratory Number 14-019

1. Introduction

The work was conducted in general accordance with the solicitation for the soil testing services for the project. The soil testing was conducted to aid in the design and construction of the taxiway and runway expansion at the Dickinson Municipal Airport.

2. Procedures

The field work was conducted on January 22 and 23, 2014. The borings were drilled at the locations staked by KLJ. A site sketch showing boring locations is included in Appendix A. The borings were backfilled on the day of drilling.

A total of 12 borings were planned for the project. Six borings were drilled for the taxiway and six borings for the runway. All twelve were accessible and drilled. The borings were drilled with standard penetration split-spoon methods, in accordance with ASTM D 1586. Soils were classified in accordance with ASTM Visual-Manual methods (ASTM D 2488). Additional information regarding drilling procedures and soils classification is given on the sheets included in Appendix A.

3. <u>Subsurface Observations</u>

Information on the subsurface conditions is given on the attached boring logs. The logs include: descriptions and classifications of soils encountered, the depths to noted soil changes, water level measurements, and soil test results. Standard penetration resistance values are given in the N columns of the logs. A sheet included in Appendix A describes symbols and descriptive terminology used on the boring logs. Also included in Appendix A is a soil classification chart.

The soil conditions encountered in this exploration may not be typical of the conditions across the site. Particularly on sites with fill, soil conditions may vary significantly within small distances.

3.1. Existing Bituminous Pavement and Aggregate Base

Bituminous pavement was encountered at the surface of six of the borings. The pavement thicknesses ranged from approximately 2.5 inches to 6.5 inches, but were generally 5 to 6 inches. The lowest measured pavement thickness was at boring 6 and was measured to be approximately 2.5 inches thick.

The aggregate base material below the pavement consisted of silty sand with a little gravel (SM). The aggregate base thicknesses ranged from approximately 6 inches to 17.5 inches, but were generally around 6 to 7 inches.

The following table lists the thicknesses of the asphalt pavement and aggregate base encountered in the borings.

Boring	Asphalt Thickness* (in.)	Agg Base Thickness* (in.)
1	n/a	n/a
2	n/a	n/a
3	n/a	n/a
4	6.0	12.0
5	n/a	n/a
6	2.5	6.0
7	6.5	17.5
8	n/a	n/a
9	5.25	7.0
10	5.25	7.0
11	n/a	n/a
12	6.0	6.0

^{*}Measurements are approximate

3.2. Subgrade Soils

Fill was encountered below the pavement and aggregate base layers in all of the borings that extended through the pavement (boring 4, 6, 7, 9, 10, and 12). Fill soils were also identified in all of the remainder of the borings except boring 1. The fill consisted of mostly sandy lean clay (CL) and clayey sand (SC) that contained pockets of topsoil. The fill in boring 6 consisted of mostly silty sand (SM) and sandy fat clay (CH). The depth of fill encountered ranged from approximately 2 feet to 6.5 feet. Borings 3, 5, and 11 encountered a surficial layer of topsoil (OL) fill. Boring 1 encountered a surficial layer of topsoil that extended to approximately 2 feet below the surface.

The following table represents the amount of fill and topsoil encountered in the borings.

Boring	Depth to Bottom of Topsoil (feet)	Depth to Bottom of Fill (feet)
1	2.0	n/a
2	n/a	4.0
3	1.0	3.0
4	n/a	6.5
5	0.6	6.5
6	n/a	3.0
7	n/a	5.5
8	n/a	2.0
9	n/a	5.5
10	n/a	4.0
11	0.5	2.0
12	n/a	4.0

^{*}Layer of topsoil below fill.

Generally, below the fill and at depths greater than 3 to 4 feet below the surface, the naturally deposited soils consisted of mostly fat clay (CH) and shale with a textural classification of fat clay. The clays contained some lenses and laminations of silt and sand,

with notable layers of silty sand (SM) and sand with silt (SP-SM) in borings 1, 3, and 6. Other notable naturally deposited soil types encountered in our exploration included clayey sand (SC) (borings 1, 5, and 11), silty clay (CL-ML) (borings 3 and 8), and lean clay (CL) (boring4). Based on the standard penetration resistance ("N") values, the natural clays ranged from soft to very hard, but were generally firm to hard in consistency. The natural deposited sands and with silts were generally medium dense to dense in consistency.

No cobbles and boulders were encountered during drilling. However boulders and cobbles could be encountered during excavations.

3.3. Groundwater

Groundwater measurements were taken at the completion of drilling. No groundwater entered any of the borings prior to backfilling.

Water levels can be expected to fluctuate both yearly and seasonally. The water levels at the time of construction may differ significantly from those encountered during our exploration program. Long term monitoring of the groundwater was not included in the scope of services.

4. Laboratory Evaluation

The soil samples obtained and classified in the field were returned to the laboratory and examined for verification of the field classification. After reviewing the soils, in-situ moisture contents were determined on selected soil samples at depths greater than one foot below the ground surface. Moisture content tests were conducted on the subgrade soils. The moisture contents ranged from 13% to 22% on the clay samples. One test performed on a silty sand tested 9% moisture. Moisture test results to the nearest 1 percent are noted on the attached boring logs.

Three composite bulk samples of the clayey subgrade soils were tested for particle-size, Atterberg limits, moisture-density relationship, and laboratory California Bearing Ratio (CBR). Soils for Bulk 1 were collected from 4 to 7 feet in borings 1, 2, 3, and 5; soils for Bulk 2 were collected from borings 6 and 11 from 1 to 5 feet; and soils for bulk 3 were collected from borings 10 and 12 from depths of 2 to 5 feet. Three CBR points were tested for each sample. For each set, the soil was remolded to approximately 95% of standard Proctor density (ASTM D 698) at moisture contents of 3% below optimum, at optimum, and 3% above optimum moisture content. The CBR penetration tests were performed after the 96 hour soaking for swell determination. The test report sheets are attached in Appendix B.

The lowest CBR values were achieved when remolded below and above optimum moisture. The highest values were achieved when remolded near the optimum moisture content. Generally, swell increased with lower initial moisture contents and changes in moisture content after soaking were also greatest when soils were remolded at lower moisture contents.

The following is a summary of the subgrade test results:

Sample No.	Soil. Class	Max Density	Opt. Moist.	LL	PL	PI	CBR 0.1 pen	CBR 0.2 pen
<u>Bulk 1</u>	CL	111.2	16.2	30	14	17		
-3%			-				2.9	2.7
at							4.7	4.1
+3							2.9	2.5
Bulk 2	CL	108.7	18.0	39	18	21		
-3%							1.4	1.4
at							4.1	4.1
+3							2.9	2.7
Bulk 3	CL	107.1	19.3	. 46	17	29		
-3%							2.3	1.8
at							3.3	2.8
+3				,			3.0	2.5

5. Conclusions and Recommendations

5.1. Existing Subgrade Conditions

The existing non-organic soils on the site are considered poor to fair as subgrade soils for pavements. In addition, the subgrade soils are frost susceptible; therefore, some frost movement and/or frost damage can be expected during the life of the pavement. Since the existing subgrade soils are susceptible and will soften due to moisture and frost penetration, it is imperative that adequate drainage be provided/maintained to remove surface water that could penetrate the surface.

It is our understanding that the existing pavement has performed satisfactorily and therefore the subgrade has also performed satisfactorily. We assumed that the subgrade below the aggregate base was prepared and the existing fill was placed with compaction control. Judging from laboratory tests, we estimate that the in-situ CBR values of existing subgrade soils below the aggregate base range from approximately 2.0 to 3.0. Based on the soil conditions encountered in the borings, laboratory tests and our experience with similar soils, it is our opinion that a maximum design CBR value of 2.5 should be used for the existing subgrade conditions.

5.2. Areas To Be Expanded or Reconstructed

If there are areas to be expanded or removed and reconstructed, the subgrade should be prepared as described below.

Again, since the existing subgrade soils are frost susceptible and will soften due to moisture and frost penetration, it is imperative that adequate drainage be provided/maintained to remove surface water that could penetrate the surface. Care should also be taken during construction to prevent excessive drying or wetting of the subgrade soils prior to surfacing.

In new construction areas, topsoil should be removed from the surface. In areas to be reconstructed, we assume that the pavement and aggregate base material will be removed and salvaged. Once the topsoil or surfacing is removed, the exposed subgrade should then be thoroughly scarified and disked a minimum of six inches deep and moisture conditioned to between 2 percent below and 2 percent above optimum. The soils should then be compacted to at least 95 % of standard Proctor density (ASTM D 698). In addition, the subgrade should be proof rolled with a heavy wheeled vehicle (such as a loaded dump truck) to detect soft spots. Soft spots should be stabilized prior to placing new fill or base course.

Based on the data reviewed, the Asphalt Institute Manual MS 1 and our experience with similar projects, we recommend that a CBR value of 2.5 be used for the existing clayey subgrade soils.

All fills and fill operations for the project should be evaluated by a qualified soils engineering firm prior to and during placement.

If earthwork is done during periods of freezing temperatures, we recommend protecting the fill from freezing once it has been placed. No frozen soils should be used as fill and fill should not be placed on frozen ground. Earthwork could be difficult in the spring or late fall when conditions are often cool and wet.

The existing subgrade soils were generally sandy lean clays (CL). From past experience, these types of subgrade soils can become very soft and unstable in the spring when frost is coming out of the ground. Particularly if site work is performed in spring or early summer, it may be necessary to scarify and rework more than the 6 inches to stabilize the subgrade and provide a stable platform for new fill or pavements.

This report was written by:

Jake Wieland, EIT

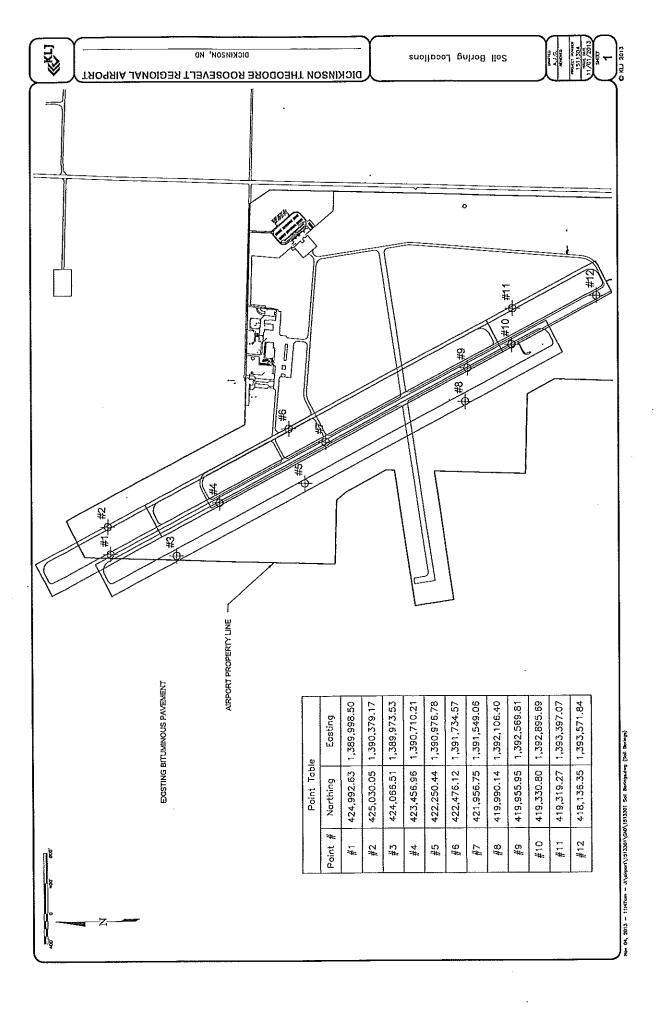
This report was reviewed by:

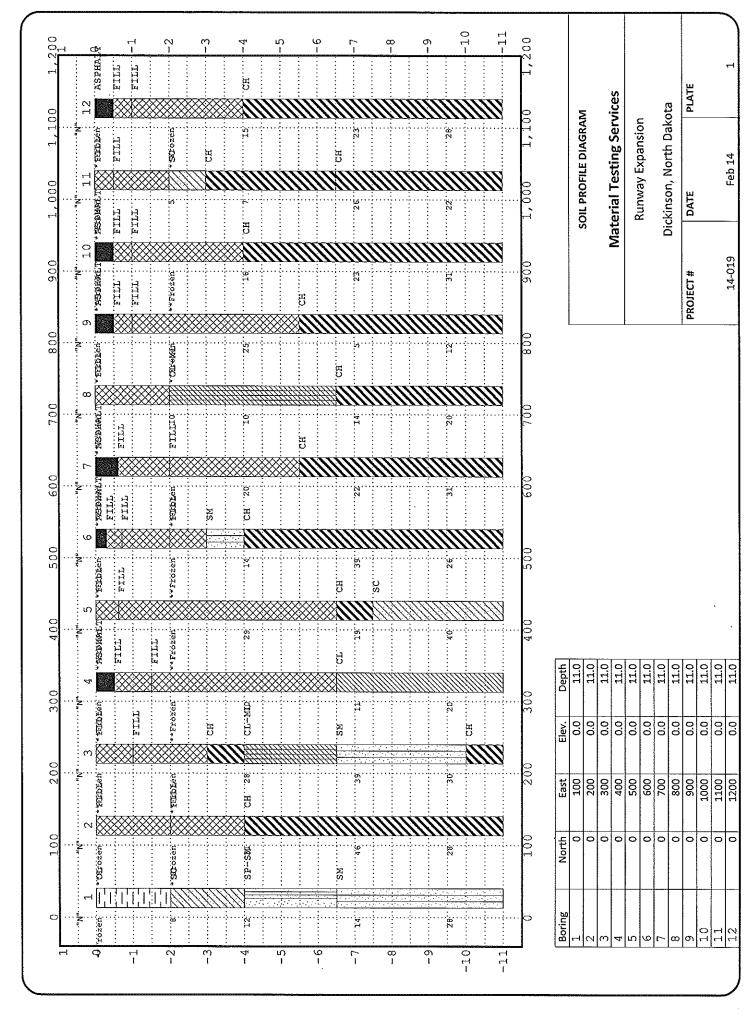


Rusten R.L. Roteliuk, PE

Appendix A

Site Sketch
Profile and Boring Logs
Symbols and Descriptive Terminology used on Logs
Soil Classification Chart





Minot, North Dakota 58702 (701) 852-5553

SOIL BORING RECORD

BORING NUMBER

START DATE

PROJECT PROJECT NUMBER

1 SHEET 1 OF 1 **Runway Expansion** PROJECT LOCATION Dickinson, North Dakota

> 14-019 1/22/14

FINISH DATE 1/22/14

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4.0			5.0-	Coarse Alluv	ium	SB			12						
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MATERIAL TESTING SERVICES, LLC Box 634 Minot, North Dakota 58702 (701) 852-5553

SOIL BORING RECORD

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Runway Expansion PROJECT LOCATION Dickinson, North Dakota

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SOIL BORING RECORD

BORING NUMBER

PROJECT PROJECT NUMBER

3 SHEET 1 OF 1 **Runway Expansion** PROJECT LOCATION Dickinson, North Dakota

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Appendix B - Report of Preliminary Soil Testing

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Minot, North Dakota 58702 (701) 852-5553

SOIL BORING RECORD

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Runway Expansion PROJECT LOCATION Dickinson, North Dakota

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FINISH DATE 1/22/14

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MATERIAL TESTING SERVICES, LLC Box 634 Minot, North Dakota 58702 (701) 852-5553

SOIL BORING RECORD

BORING NUMBER PROJECT

PROJECT NUMBER

START DATE

5 SHEET 1 OF 1 **Runway Expansion** PROJECT LOCATION Dickinson, North Dakota

14-019 1/22/14

FINISH DATE 1/22/14

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SOIL BORING RECORD

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Runway Expansion PROJECT LOCATION Dickinson, North Dakota

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Runway Expansion

PROJECT LOCATION Dickinson, North Dakota

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SHEET 1 OF 1

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11.0	1	-10.0		· · · · · · · · · · · · · · · · · · ·		\bigwedge						
	NM = None Measurable											
DRILL METHO LOGGE REVIE	D 4" FA R HD WER JW	WATER LEVEL	MEASUREMENTS	DATE TIME 1/22/2014 1555	SAMPL DEPT		CASING DEPTH	CAVE-IN DEPTH 10.9		LEVEL	L	ATER EVEL NM
DRILL	RIG CME 45	, s	×			Арр	endix B - R	eport of P	relimina	ıry Soil	Test	ng

Minot, North Dakota 58702 (701) 852-5553

SOIL BORING RECORD

BORING NUMBER PROJECT

PROJECT NUMBER

PROJECT LOCATION

8

SHEET 1 OF 1

Runway Expansion Dickinson, North Dakota

14-019 1/22/14

	SOIL BORING RECOR	D		START	T NUMB DATE	- -		-019 22/14	F	INIS	H DA	TE	1/2	2/14	
T)		ტ	\					SAM	PLE			Т	EST I	RESUL	TS
LAYER DEPTH/ ELEVATION (FT)	SOIL DESCRIPTION	SYMBOLIC LOG	ELEVATION/	GEOLOG	3Y	TYPE	LEGEND	D (pcf)	N VALUES	BLOWS/FT	WATER LEVEL	MOISTURE CONTENT(%)	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	Qu (psf)
	Fill, mostly Sandy Lean Clay, brown and dark		0.8-	Fill		SB	1		*Fro	zer				:	
2.0	Silty Clay, light brown, lenses and laminations of silt, frozen to 3' then moist, firm, (CL-ML)		-	Fine Alluvium		SB			10)		22			
6.5			5.0			SB		ANALASA ANALAS	10)					and for a face of a face of the face of th
-6.5	Shale, highly weathered, light brown with rust color mottling, lenses and laminations of silt and silty sand, moist, firm to hard, (Textural Classification: Fat Clay (CH))		- - -	Golden Valley Formation		SB			14	1					Versioniste Versioniste des constantes de la constante de la constante de la constante de la constante de la c
11.0			-10.0			SB	\bigvee		2()					TO THE TOTAL AND A STATE OF THE TOTAL AND A ST
11.0 -11.0	End of Boring		_				/ \								<u> </u>
	NM = None Measurable							APPERENT APPENDIQUE AP							
DRILL	er CW	<u>l</u>			s	AMPLE	D.	CASIN	G C	AVE-	IN	DRIL	LING	พ	ATER
METEO	*** == :		VEL	DATE		DEPTH		DEPTE	- 1	DEPT	ł	MUD I		1	EVEL
LOGGE	TID		WATER LEVEL MEASUREMENTS	1/22/2014	1455	11	4		_	10.5	5				NM
REVIE			WATE		ļ <u>.</u>		-		-		_			-	
	RIG CME 45		1 - X	· •			1_							-	

MATERIAL TESTING SERVICES, LLC Box 634 Minot, North Dakota 58702 (701) 852-5553

SOIL BORING RECORD

BORING NUMBER

PROJECT PROJECT NUMBER

Runway Expansion PROJECT LOCATION Dickinson, North Dakota

14-019 1/22/14 SHEET 1 OF 1

	SOIL BORING RECORD			1.1	ECT NUM T DATE	BER		1-019 22/14	FI	NISH	DATE	1/2	2/14	
	(7)				· · · · · · · · · · · · · · · · · · ·			SAM	IPLE			TEST	RESUL	TS
LAYER DEPTH/ ELEVATION (FT)	SOIL DESCRIPTION SAMBOLIC	ELEVATION/		GEOL	ЭGY	TYPE	LEGEND	D (pcf)	N VALUES	BLOWS/FT WATER	LEVEL MOISTURE	10°	PLASTIC LIMIT (%)	Qu (psf)
0.5	5.25" Asphalt	. 0	اً ٥.	Fill		SB	1		**Fro	zer				
0.5 -0.5 1.0 -1.0	7" Base-Course, mostly Silty Sand, dark brown, a little gravel, fine to coarse grained sand, frozen, (SM) Fill, mostly Sandy Lean Clay, brown and dark brown mixed, a little gravel, traces of topsoil, a few asphalt fragments, frozen to 4" then moist, (CL) Shale, highly weathered, light brown, numerous lenses and laminations of silt, moist, soft to firm, (Textural Classification: Fat Clay (CH)) End of Boring	5	50.	Golden Valle Formation	ey.	SB SB			**Fro					
:	NM = None Measurable	!	******											
				· · · · · · · · · · · · · · · · · · ·	·		Ц					<u></u>		
DRILL		13	SE	DATE	TIME	SAMPLE DEPTE		CASIN DEPTH		VE-IN EPTH	1	LLING LEVEL		ATER EVEL
METHO	TTT	WATER LEVEL	MEASUREMENTS	1/22/2014	1630	11			_	11.1	1			МИ
LOGGE	THE	TER	SOR											
DRILL	C1 FD 4#	8	MEA											
				***************************************		,	Appe	endix B	- Repo	ort of F	relimin	ary Sc	oil Tes	ting

Minot, North Dakota 58702 (701) 852-5553

SOIL BORING RECORD

BORING NUMBER PROJECT

PROJECT NUMBER

START DATE

10 SHEET 1 OF 1 **Runway Expansion** PROJECT LOCATION Dickinson, North Dakota

14-019 1/22/14

FINISH DATE 1/22/14

SOIL BORING RECORD		START DATE		1/.	22/14	FINIS	H DA	AIE	1/22	/14	
\(\hat{H}\)					SAMP	'LE		T	EST F	ESUL	TS
LAYER DEPTH/ ELEVATION (FT) SOIT DESCRIBATION (FT) SYMBOLIC LOG	ELEVATION/ DEPTH (FT)	GEOLOGY	TYPE	LEGEND	D (pcf)	N VALUES BLOWS/FT	WATER LEVEL	MOISTURE CONTENT(%)	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	Qu (psf)
0.5 5.25" Asphalt	0.0-	Fill	SB	6	* :	*Frozei					
7" Base-Course, mostly Silty Sand, dark brown, a little gravel, fine to coarse grained sand, frozen, (SM) Fill, mostly Sandy Lean Clay, brown and dark brown mixed, a trace of gravel, traces of topsoil, frozen, (CL)	-		SB		The contract of the contract o	*Frozer		16		ABLE COMMENTED TO THE COMMENT OF THE	
4.0 -4.0 Shale, highly weathered, light brown, numerous lenses and laminations of silt and silty sand, dry to moist, hard to very hard, (Textural Classification: Fat Clay (CH))	-5.5-	Golden Valley Formation	SB			16					
			SB	\bigvee		23					
11.0	-10.0-		SB	\setminus		31		A de la companya de l			
NM = None Measurable	-										
DRILLER CW METHOD 4" FA LOGGER HD REVIEWER JW	WATER LEVEL		SAMPLE DEPTH		CASING DEPTH	CAVE- DEP:	СН	DRIL MUD I		LF	ATER EVEL NM
DRILL RIG CME 45	WA KE		7	App	endix B -	Report	of Pre	elimina	iry So	l Tesi	ting

MATERIAL TESTING SERVICES, LLC Box 634 Minot, North 928,6523 58702

(701) 852-5553

SOIL BORING RECORD

BORING NUMBER PROJECT

START DATE

PROJECT NUMBER

11 SHEET 1 OF 1 **Runway Expansion** PROJECT LOCATION Dickinson, North Dakota

> 14-019 1/23/14

FINISH DATE 1/23/14

				STAKT DATE			20/14		311107		1/20		
/ T)		O					SAM	PLE		Т	EST F	RESUL	TS
LAYER DEPTH/ ELEVATION (FT)	SOIL DESCRIPTION	SYMBOLIC LOG	ELEVATION/	GEOLOGY	TYPE	TEGEND	D (pcf)	N VALUES BLOWS/FT	WATER	MOISTURE CONTENT (%)	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	Qu (psf)
٠.	Fill, mostly Organic Lean Clay, dark brown,	XX	0.8-	Fill	SB	1		**Froze	ī.				
0.5	frozen, (OL) <u>Fill, mostly Sandy Lean Clay</u> , brown and dark brown mixed, a few fine roots, traces of topsoil, frozen, (CL)									-			
2.0 -2.0	Clayey Sand, brown to light brown,		-	Mixed Alluvium	SB	ackslash		5	and the state of t				
-3.0	Fat Clay, light brown, numerous lenses and laminations of silt, frozen to 4' then moist, soft, (CH)			Fine Alluvium	SB			7					
6.5 -6.5	Shale, highly weathered, light brown, numerous lenses and laminations of silt, moist, hard, (Textural Classification: Fat Clay (CH))		-5.0	Golden Valley Formation	SB			26				- The state of the	
11.0			-10 ¹⁰		SB			22					
-11.0	End of Boring NM = None Measurable											ANNOMEN REPRESENTATION OF THE PROPERTY OF THE	
	ER CW	<u> </u>	T		SAMPLI	ED	CASI	G CAVI	 -IN	DRII	LING	W W	ATER
DRILL	(4) 73 3		VEL		DEPT		DEPT	1	1		LEVEL	ŧ	EVEL
LOGGE	TTD		WATER LEVEL	1/23/2014 1100	11			10	.4				им
REVIE			WATE						***************************************				
DRILL	RIG CME 45					Δnn	andiy D	- Report	of Pro	limina	ny So	ii Too	ting
					,	-t 1 ()	X B	- 5000	16			_	

MATERIAL TESTING SERVICES, LLC Box 634 Minot, North Dakota 58702 (701) 852-5553

SOIL BORING RECORD

BORING NUMBER **PROJECT**

PROJECT LOCATION

PROJECT NUMBER

START DATE

SHEET 1 OF 1 **Runway Expansion** Dickinson, North Dakota

14-019 1/22/14

12

FINISH DATE 1/22/14

SAMPLE TEST RESULTS LAYER DEPTH/ ELEVATION/ DEPTH (FT) MOISTURE CONTENT(%) N VALUES BLOWS/FT SYMBOLIC ELEVATION (pcf) LEGEND TYPE SOIL DESCRIPTION **GEOLOGY** g 0.0 6" Asphalt Fill SB *Frozer 0.5 -0.5 6" Base-Course, mostly Silty Sand, dark 1.0 brown, a little gravel, fine to coarse grained sand, frozen, (SM) Fill, mostly Sandy Lean Clay, brown and dark brown mixed, a trace of gravel, pockets of fat clay, traces of topsoil, frozen, (CL) ŞВ *Frozen 35 14 Shale, highly weathered, light brown, Golden Valley SB 15 numerous lenses and laminations of silt and silty Formation sand, moist, firm to hard, (Textural -5.0 5.0 Classification: Fat Clay (CH)) ŞB 23 SВ 28 -10.011.0 -11.0End of Boring NM = None Measurable SAMPLED CASING CAVE-IN DRILLING WATER CW DRILLER MEASUREMENTS WATER LEVEL DATE TIME DEPTH DEPTH MUD LEVEL LEVEL 4" FA METHOD /22/201 1725 11 10.8 NM HDLOGGER JW REVIEWER DRILL RIG **CME 45**

SYMBOLS AND DESCRIPTIVE TERMINOLOGY ON TEST BORING LOG

SYMBOLS FOR DRILLING AND SAMPLIN	(G	SYMBOLS FOR LABORATORY TESTS
Symbol Description	Symbol W D LL PL Qu Pq Ts G SL OC SP PS FS SS pH SC CC C* Qe* Qe* D.S.* K* DH* MA* R E* PM* VS* IR* RQD	Description Water content Dry density - pounds per cubic foot Liquid limit - ASTM** D 4318 Plastic limit - ASTM D 4318 Inserts in Last Column (Qu or RQD) — Unconfined compressive strength, psf - ASTM D 2166 Penetrometer reading, tsf Torvane reading, tsf Specific gravity Shrinkage limits - ASTM D 427 Organic content - Combustion method Swell pressure, tsf Percent swell under pressure Free swell, percent Shrink swell, percent Hydrogen ion content - Meter Method Sulfate content, parts/million or mg/l Chloride content, parts/million or mg/l One dimensional consolidation - ASTM D 2435 Triaxial compression Direct shear - ASTM D 3080 Coefficient of permeability, cm/sec Double hydrometer - ASTM D 4221 Particle size analysis - ASTM D 422 Laboratory electrical resistivity, ohm-cm - ASTM G 57 Pressuremeter deformation modulus, tsf Pressuremeter test Field vane shear - ASTM D 2573 Infiltrometer test - ASTM D 3385 Rock quality designation, percent Results shown on attached data sheet or graph ASTM designates American Society for Testing and Materials

DESCRIPTIONS OF N-VALU	ES VS. SOIL P	ROPERTIES	DESCRIPTIONS OF SOIL CONDITIONS			
N Value Density 0 - 4 Very loose 5 - 10 Loose 11 - 30 Medium dense 31 - 50 Dense Over 50 Very dense	N Value 0 - 4 5 - 8 9 - 15 16 - 30 Over 30	Consistency Very soft Soft Firm Hard Very hard	Condition Lamination Layer Dry Moist Wet Waterbearing Varved	Description Up to 1/2" thick stratum 1/2" to 6" thick stratum Powdery, no noticeable water Below saturation Saturated, above liquid limit Pervious soil below water Alternating laminations of any combinations of clay, silt and fine grained sand		

L	DESCRIPTIONS OF GRA	AVEL PROPORTION:	S IN SOILS	DESCRIPTIONS OF PARTICLE SIZES			
	Soil Type Coarse grained soils	Description A little gravel	Range, %	Material Type Boulders	Size Over 12"		
	Coarse grained soils	With gravel	15 - 49	Cobbles	3" - 12"		
	Fine grained soils:			Coarse gravel Fine gravel	3/4" - 3" #4 sieve - 3/4"		
	71-85% passing #200 sieve	A little gravel	2 - 7	Coarse sand	#4 - #10 sieve		
	71-85% passing #200 sieve	With gravel	8 - 29	Medium sand	#10 - #40 sieve		
	70% passing #200 sieve	A little gravel	2 - 14	Fine sand	#40 - #200 sieve		
1	70% passing #200 sieve	With gravel	15 - 24	Silt	100% passing #200 sieve and > 0.002mm		
L	70% passing #200 sieve	Gravelly	16 - 49	Clay	100% passing #200 sieve and < 0.002mm		

c:\wpwin\forms\desc

SOIL CLASSIFICATION CHART

4.2	A IOB BUILDI	3110	SYM	BOLS	TYPICAL
IVI.	AJOR DIVISION	GRAPH	LETTER	DESCRIPTIONS	
	GRAVEL	CLEAN GRAVELS		GW	WELL-GRADED GRAVELS, GRAVEL - SAND MIXTURES, LITTLE OR NO FINES
	AND GRAVELLY SOILS	(LITTLE OR NO FINES)		GP	POORLY-GRADED GRAVELS, GRAVEL - SAND MIXTURES, LITTLE OR NO FINES
COARSE GRAINED SOILS	MORE THAN 50% OF COARSE FRACTION	GRAVELS WITH FINES		GM	SILTY GRAVELS, GRAVEL - SAND - SILT MIXTURES
	RETAINED ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		GC	CLAYEY GRAVELS, GRAVEL - SAND - CLAY MIXTURES
	SAND	CLEAN SANDS		sw	WELL-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES
MORE THAN 50% OF MATERIAL IS LARGER THAN NO. 200 SIEVE SIZE	AND SANDY SOILS	(LITTLE OR NO FINES)		SP	POORLY-GRADED SANDS, GRAVELLY SAND, LITTLE OR NO FINES
	MORE THAN 50% OF COARSE FRACTION	SANDS WITH FINES		·SM	SILTY SANDS, SAND - SILT MIXTURES
·	PASSING ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		sc	CLAYEY SANDS, SAND - CLAY MIXTURES
				ML	INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS OR CLAYEY SILTS WITH SLIGHT PLASTICITY
FINE GRAINED	SILTS AND CLAYS	LIQUID LIMIT LESS THAN 50		CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS
SOILS	7-2			OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY
MORE THAN 50% OF				МН	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE SAND OR SILTY SOILS
4] 200 OIL 4L OILL	SILTS AND CLAYS	LIQUID LIMIT GREATER THAN 50		СН	INORGANIC CLAYS OF HIGH PLASTICITY
< ort-ormali(<sk)owo>></sk)owo>	·			ОН	ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS
	GHLY ORGANIC S	SOILS	77 77 77 77 7 77 77 77 77 77 77 77 77	PT	PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS

NOTE: DUAL SYMBOLS ARE USED TO INDICATE BORDERLINE SOIL CLASSIFICATIONS

Appendix B

Laboratory Test Reports

P.O. Box 634 Minot, ND 58702 (701) 852-5553

CALIFORNIA BEARING RATIO - ASTM 1883

P.O. Box 1093 Williston, ND 58802 (701) 572-4226

RUNWAY EXPANSION

DATE:

PROJECT:

DICKINSON MUNICIPAL AIRPORT

DICKINSON, NORTH DAKOTA

18-Feb-14

REPORTED TO:

KLJ

128 Soo Line Drive

Bismarck, ND 58501-3310

Laboratory Number

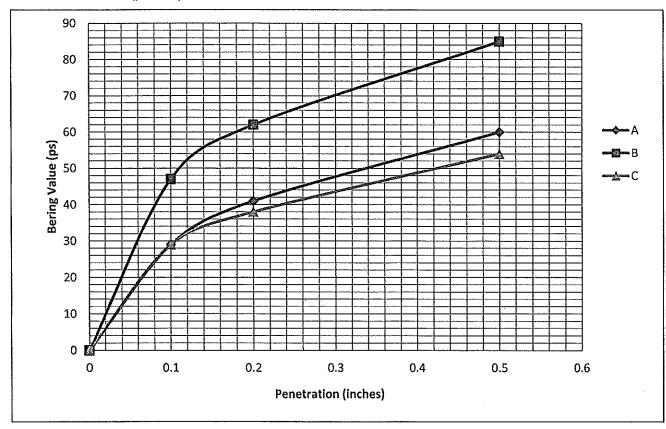
14-019

SAMPLE IDENTIFICATION:

Bulk 1, auger cuttings, borings 1,2,3,5; 4 to 7 feet

SOIL DESCRIPTION: SANDY LEAN CLAY (LL-30, PL-14, PI-17)

MOISTURE-DENSITY RELATION: (ASTM D 698)	Maximum Dry Optimum Moi	111.2 16.2	pcf %	
TEST TRIAL: Dry Density, at molding Moisture Content, at molding % of Maximum Dry Density	A (-3) 105.6 13.4 95.0	B (at) 105.5 16.4 94.9	C (+3) 106.2 19.4 95.5	
Moisture Content after soaking CORRECTED BEARING RATIO: at 0.1" penetration	19.4 2.9	19.3 4.7	19.9 2.9	
at 0.1" period attorn at 0.2" penetration SWELL, % of initial heights	2.7 2.36	4.1 0.84	2.5 0.40	
SURCHARGE WEIGHT (pounds):	12.55	12.70	12.45	



P.O. Box 634 Minot, ND 58702 (701) 852-5553

CALIFORNIA BEARING RATIO - ASTM 1883

P.O. Box 1093 Williston, ND 58802 (701) 572-4226

PROJECT:

RUNWAY EXPANSION

DATE:

18-Feb-14

REPORTED TO:

KLJ

128 Soo Line Drive Bismarck, ND 58501-3310

DICKINSON MUNICIPAL AIRPORT DICKINSON, NORTH DAKOTA

Laboratory Number

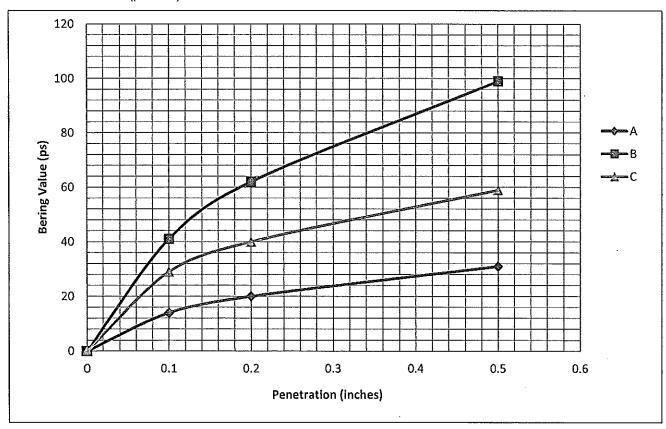
14-019

SAMPLE IDENTIFICATION:

Bulk 2, auger cuttings, borings 6, 11; 1 to 5 feet

SOIL DESCRIPTION: LEAN CLAY with SAND (LL-39, PL-18, PI-21)

MOISTURE-DENSITY RELATION:	Maximum Dry	Density	108.7	pcf
(ASTM D 698)	Optimum Moi	18.0	%	
TEST TRIAL:	A (-3)	B (at)	C (+3)	
Dry Density, at molding	102.4	104.9	103.0	
Moisture Content, at molding	15.0	18.0	21.0	
% of Maximum Dry Density	94.2	96.5	94.8	
Moisture Content after soaking	22.8	21.7	22.3	
CORRECTED BEARING RATIO:				
at 0.1" penetration	1.4	4.1	2.9	
at 0.2" penetration	1.4	4.1	2.7	
SWELL, % of initial heights	5.11	1.38	0.78	
SURCHARGE WEIGHT (pounds):	12.51	12.53	12,55	



P.O. Box 634 Minot, ND 58702 (701) 852-5553

CALIFORNIA BEARING RATIO - ASTM 1883

P.O. Box 1093 Williston, ND 58802

RUNWAY EXPANSION

DATE:

(701) 572-4226

PROJECT:

DICKINSON MUNICIPAL AIRPORT

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128 Soo Line Drive

DICKINSON, NORTH DAKOTA

Bismarck, ND 58501-3310

Laboratory Number

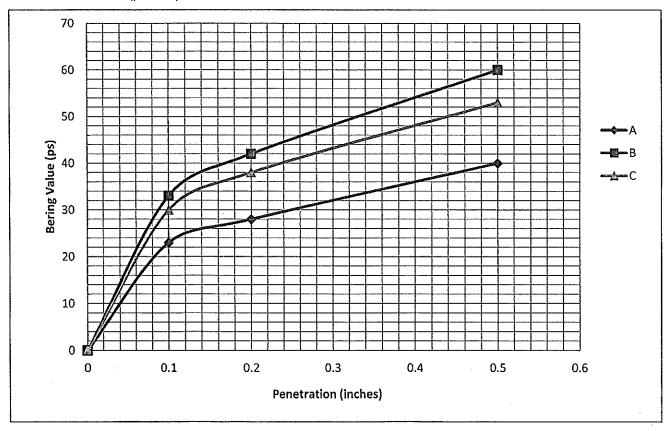
14-019

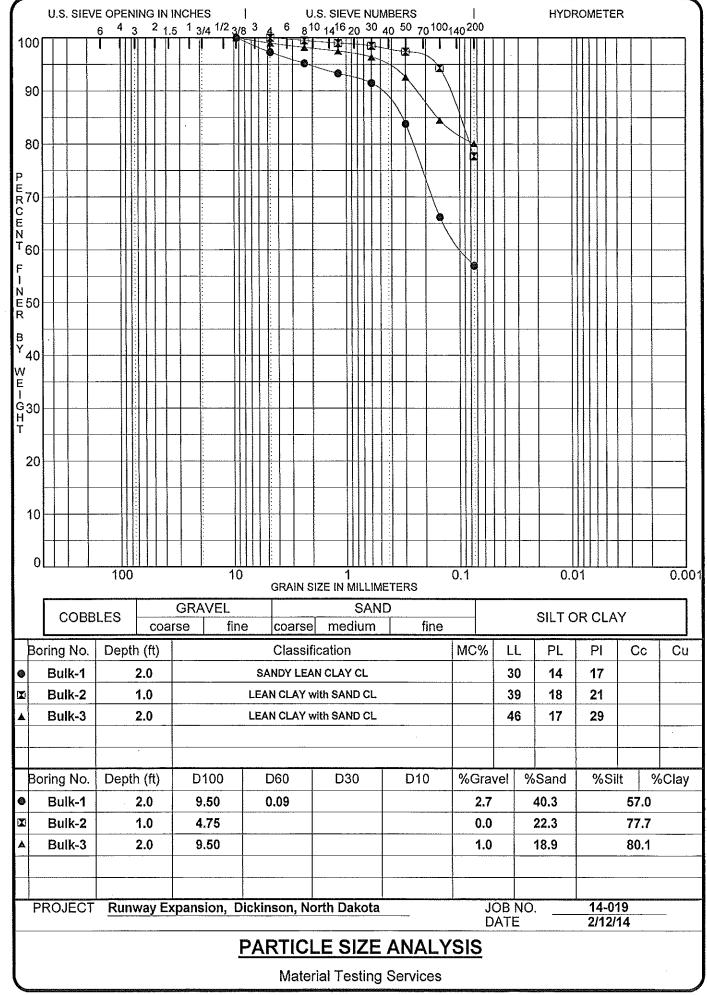
SAMPLE IDENTIFICATION:

Bulk 3, auger cuttings, borings 10, 12; 2 to 5 feet

SOIL DESCRIPTION: LEAN CLAY with SAND (LL-46, PL-17, PI-29)

MOISTURE-DENSITY RELATION: (ASTM D 698)	Maximum Dry Optimum Moi	107.1 19.3	pcf %	
TEST TRIAL:	A (-3)	B (at)	C (+3)	
Dry Density, at molding	101.7	101.4	101.7	•
Moisture Content, at molding	16.3	19.3	22.3	
% of Maximum Dry Density	94.9	94.6	95.0	
Moisture Content after soaking	23.6	23.2	24.1	
CORRECTED BEARING RATIO:				
at 0.1" penetration	2.3	3.3	3.0	
at 0.2" penetration	1.8	2.8	2.5	
SWELL, % of initial heights	4.04	1.93	0.33	
SURCHARGE WEIGHT (pounds):	12.51	12.53	15.65	





P.O. Box 634 Minot, ND 58702 (701) 852-5553

MOISTURE-DENSITY RELATIONSHIP

P.O. Box 1093 Williston, ND 58802 (701) 572-4226

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DICKINSON MUNCIPAL AIRPORT

DICKINSON, NORTH DAKOTA

DATE:

17-Feb-14

COPIES TO:

REPORTED TO:

KLJ

128 Soo Line Drive Bismarck, ND 58501-3310

Laboratory Number

14-019

Sample Number:

Bulk 1

Sample ID:

borings 1, 2, 3, 5; 4 to 7 feet

tested 2/4/2014

Soil Description:

SANDY LEAN CLAY

Unified Soil Classification:

CL

Results:

Method

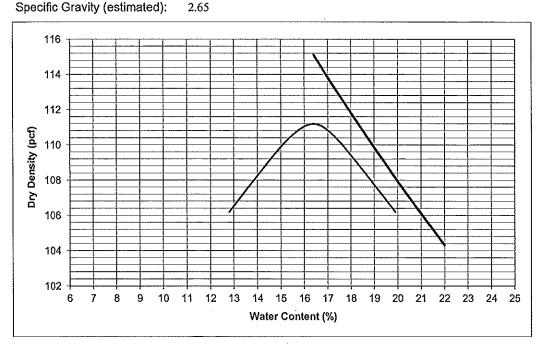
ASTM D 698, Method B

Maximum Dry Density

Optimum Moisture Content

111.2 pcf % 16.4

2.65



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MOISTURE-DENSITY RELATIONSHIP

P.O. Box 1093 Williston, ND 58802 (701) 572-4226

PROJECT:

RUNWAY EXPANSION

DICKINSON MUNCIPAL AIRPORT

DICKINSON, NORTH DAKOTA

DATE:

17-Feb-14

COPIES TO:

REPORTED TO:

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128 Soo Line Drive Bismarck, ND 58501-3310

Laboratory Number

14-019

Sample Number:

Bulk 2

Sample ID:

borings 6, 11; 1 to 5 feet

tested 2/4/2014

Soil Description:

LEAN CLAY with SAND

Unified Soil Classification:

CL

Results:

Method

ASTM D 698, Method B

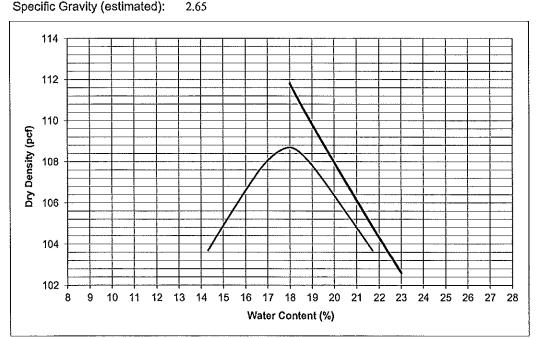
Maximum Dry Density

pcf 108.7

Optimum Moisture Content

18.0 %

Specific Gravity (estimated):



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RUNWAY EXPANSION

DICKINSON MUNCIPAL AIRPORT

DICKINSON, NORTH DAKOTA

DATE:

17-Feb-14

COPIES TO:

REPORTED TO:

KLJ

128 Soo Line Drive Bismarck, ND 58501-3310

Laboratory Number

14-019

Sample Number:

Bulk 3

Sample ID:

borings 10, 12; 2 to 5 feet

tested 2/4/2014

Soil Description:

LEAN CLAY with SAND

Unified Soil Classification:

CL

2.65

Results:

Method

ASTM D 698, Method B

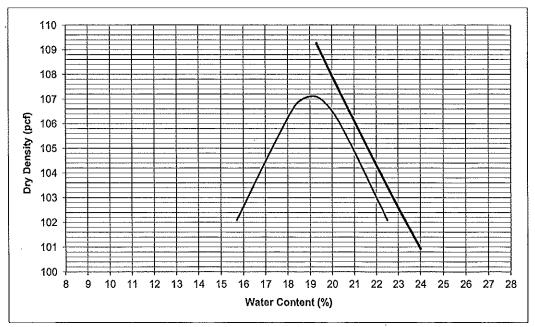
Maximum Dry Density

107.1 pcf

Optimum Moisture Content

% 19.3

Specific Gravity (estimated):



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